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Original Research Article

Hybrid metaheuristic optimization and comparative analysis of InGaAs/InP quantum well infrared photodetector for enhanced performance

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ABSTRACT

This work presents a hybrid metaheuristic optimization and comparative analysis of an InGaAs/InP-based quantum well photodetector (QWP) designed for terahertz (THz) long-wavelength infrared applications in the 8-12 μm spectral range. A comprehensive theoretical model is developed to enhance key performance parameters, including quantum efficiency, responsivity, detectivity, dark current, and noise equivalent power (NEP). The detector performance is strongly governed by structural parameters such as quantum well width and Indium mole fraction. Optimized results demonstrate peak absorption at 28.2 THz (10.6 μm) for a well width of 60 \AA and Indium mole fraction of 0.34. At this optimized configuration, the device exhibits a high responsivity of 2.7 A/W, enhanced detectivity of $5.38 \times 10^{11} \text{ cm}\sqrt{\text{HzW}}^{-1}$, and a low dark current of 68 nA, indicating improved sensitivity and reduced noise performance. The corresponding NEP is significantly minimized due to the high detectivity of the device. To further improve performance, a multi-objective optimization framework is implemented using several metaheuristic algorithms, including Grey Wolf Optimization, Symbiotic Organism Search, Differential Evolution, Whale Optimization, Genetic Algorithm, Particle Swarm Optimization (PSO), and Ant Colony Optimization. The optimization simultaneously maximizes quantum efficiency, responsivity, and detectivity, while minimizing dark current and NEP. A comparative analysis reveals that a hybrid NSGA-II-PSO approach provides superior convergence and optimal trade-off characteristics, demonstrating its effectiveness for advanced QWP design and next-generation THz photodetection systems. The novelty of this work lies in the hybrid optimization-driven performance enhancement of InGaAs/InP QWPs, making them highly suitable for high-sensitivity THz communication and long-wavelength infrared detection applications.

1. Introduction

Quantum Well Infrared Photodetectors (QWIPs) have been extensively studied since the pioneering work of B. F. Levine, 1993, who established the fundamental principles of intersubband transitions and device operation for infrared detection [1]. Subsequent foundational contributions by H. C. Liu et al., 2006; Durante et al., 2007, further clarified the dependence of responsivity, absorption spectrum, and photoconductive gain on quantum well design parameters, providing a strong theoretical basis for device optimization [2, 3]. These classical studies demonstrated that QWIPs offer advantages such as spectral tunability, mature fabrication technology, and compatibility with semiconductor processing [4]. However, early designs were limited by relatively high dark current, narrow bandwidth and slower response times [1, 5].

In recent years, significant progress has been made toward improving QWIP performance through advanced material systems and structural engineering. For instance, Min-Su Park et al. demonstrated InGaAs/InP-based QWIPs integrated on silicon substrates, highlighting their potential for long-wavelength infrared detection with improved lattice matching

and device uniformity [4]. Similarly, recent studies have explored broadband detection, enhanced detectivity, and reduced noise characteristics using novel heterostructures and quantum well configurations [4, 6]. Advances in modeling and simulation approaches, including TCAD-based analysis and analytical techniques, have further enabled accurate prediction and optimization of device performance [7]. Despite these developments, achieving a simultaneous improvement in responsivity, detectivity, bandwidth, and response time remains a challenging task, thereby motivating the need for systematic design and optimization of quantum well photodetectors for high-performance infrared applications.

Metaheuristic optimization techniques have recently been widely used for the design and performance enhancement of semiconductor photodetectors due to their effectiveness in handling complex, multi-parameter problems. Algorithms such as GA, PSO, DE, and GWO enable optimization of structural and material parameters to improve responsivity, detectivity, and reduce dark current. Among these, PSO offers fast convergence and ease of implementation, while GWO and DE provide higher accuracy in global optimization. Additionally, hybrid approaches combining these algorithms have been



explored to achieve better optimization efficiency and robust device performance [8–10].

In this work, an InGaAs/InP-based quantum well photodetector (QWP) is proposed for long-wavelength terahertz (THz) infrared detection in the 8–12 μm spectral range. The structure consists of an InGaAs quantum well sandwiched between InP barrier layers, forming a type-I heterostructure that provides strong carrier confinement and efficient intersubband transitions. The device performance is governed by key structural parameters such as quantum well width and Indium mole fraction, enabling precise spectral tuning. Energy states and transition characteristics are analyzed using the Transfer Matrix Method (TMM) and validated through TCAD-based simulations, ensuring both analytical and numerical accuracy. Furthermore, a hybrid metaheuristic optimization framework is employed to enhance responsivity, detectivity, and quantum efficiency while minimizing dark current and noise. The optimized structure exhibits peak operation at 28.2 THz (10.6 μm), demonstrating its suitability for high-sensitivity THz communication and long-wavelength infrared detection applications.

The novelty of this work lies in the integration of a physics-based InGaAs/InP quantum well photodetector model with a hybrid metaheuristic optimization framework for simultaneous multi-objective performance enhancement. Unlike conventional approaches that rely on parametric tuning, the proposed hybrid NSGA-II–PSO algorithm systematically identifies the optimal design parameters ($L_w = 60 \text{ \AA}$, $L_b = 400 \text{ \AA}$, $x = 0.34$), achieving an improved trade-off among responsivity, detectivity, dark current, and noise equivalent power. This combined modeling and optimization strategy enables enhanced sensitivity, faster response, and efficient long-wavelength THz detection, making the proposed device highly suitable for next-generation infrared communication systems.

The remainder of this paper is organized as follows: Section 2 presents the device structure and Theoretical formulation of the proposed InGaAs/InP QWP, Section 3 demonstrates results and discussions of hybrid NSGA-II–PSO optimization framework, Section 4 concludes the paper with key findings and future perspectives.

2. Theoretical formulation

The proposed InGaAs/InP-based QWP consists of an $\text{In}_x\text{Ga}_{1-x}\text{As}$ quantum well sandwiched between two InP barrier layers, forming a type-I heterostructure as illustrated in Figure 1. The conduction band discontinuity at the InGaAs/InP interface creates a potential well that confines electrons within the well region (region II), while the adjacent barrier regions (regions I and III) restrict carrier leakage. Under incident radiation, electrons undergo intersubband transitions from the ground state (E_1) to the excited state (E_2), generating photocurrent through tunneling or thermionic emission mechanisms. The asymmetry introduced by the applied bias further facilitates carrier transport toward the contact layer, enabling efficient photodetection in the long-wavelength terahertz regime.

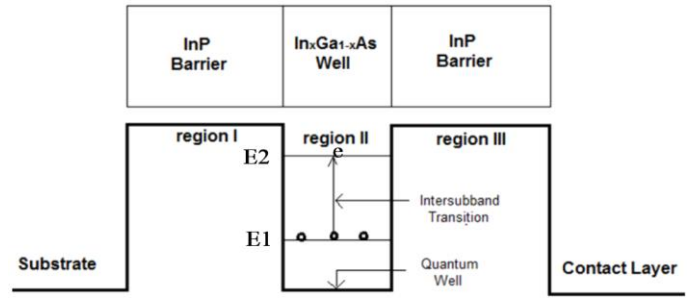


Figure 1: Energy band diagram of InGaAs/InP -based QWP [11].

2.1 Analytical modeling using the Transfer Matrix Method (TMM)

The quantized energy states of the proposed InGaAs/InP-based heterostructure, were solved by using one dimensional *Schrödinger equation* across the three regions, InP barrier (region I), InGaAs well (region II), and InP barrier (region III) as illustrated in figure 1 [12].

$$\frac{d}{dx} \left[\frac{1}{m^*(x,E)} \frac{d\psi(x)}{dx} \right] + \frac{2m^*(x,E)}{\hbar^2} [E - V(x)]\psi(x) = 0. \quad (1)$$

Here $m^*(x, E)$ represents the position dependent effective mass and $V(x)$ represents the potential profile. The Transfer Matrix Method (TMM) was employed for solving the Schrödinger equation (1).

For a wave entering from region I and exiting region III, the transmission coefficient can be approximated as:

$$\tau = \frac{|F e^{ik_1 x}|^2}{|A e^{ik_1 x}|^2} = \frac{1}{|t_{11}|^2}. \quad (2)$$

The solution of this equation gives the quantized energy eigenstates and the corresponding transition energy $\Delta E = E_2 - E_1$, further ΔE determines the absorption wavelength as

$$\lambda = \frac{hc}{\Delta E}. \quad (3)$$

2.2 Numerical modeling and transport simulation Using TCAD

The optoelectronic performance of the proposed photodetector is analyzed using a TCAD-based finite element framework. The simulator solves the coupled Poisson, carrier continuity, and drift-diffusion transport equations to describe the interaction between electrostatic potential and carrier dynamics. These governing equations are iteratively solved using the Newton-Raphson method to obtain a self-consistent solution. In the present study, a quantum well width (L_w) = 60 \AA barrier width of (L_b) = 400 \AA and Indium mole fraction of $x = 0.34$ were considered as the optimized structural parameters. The doping concentration is taken as $1.53 \times 10^{24} \text{ cm}^{-3}$ in the quantum well region and $1.33 \times 10^{21} \text{ cm}^{-3}$ in the barrier region, ensuring efficient carrier confinement and transport for enhanced device performance.

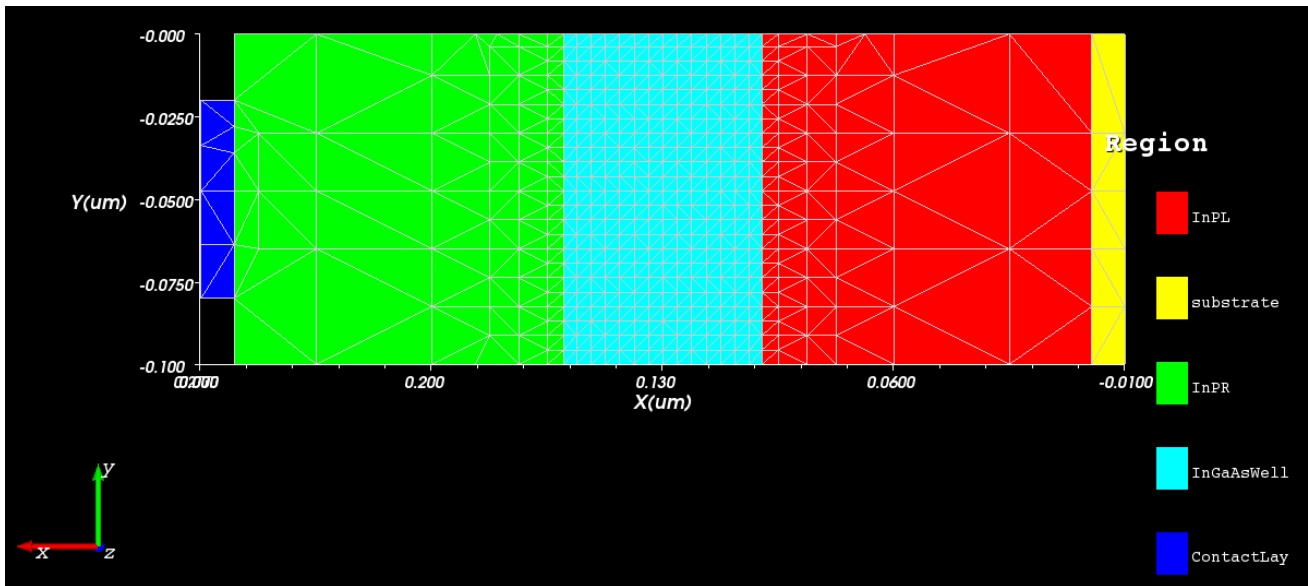


Figure 2: TCAD Simulated model of InGaAs/InP-based QWP.

Poisson's equation

The relation between charge density and electric field potential for the proposed QWP can be expressed from the Poisson's equation [7], as:

$$\rho_{\text{total}}(x) = N_{D1}(x) + N_{A2}(x) + \rho D(x) + \rho A(x) + \rho(x)_{\text{bound}} \quad (4)$$

Here N_{D1} and N_{A2} represent the donor and acceptor densities of the InP barrier and InGaAs well regions, and $\rho(x)$ is the total charge density including donor (N_{D1}) and acceptor (N_{A2}) contributions respectively.

Continuity equation

The continuity equations for electron and hole can be expressed as

$$\begin{aligned} \mathcal{D}n \frac{d^2 n(y)}{dy^2} - \wp(y) + G_{l,q} &= 0 \quad \text{and} \\ \mathcal{D}p \frac{d^2 p(y)}{dy^2} - \wp(y) + G_{l,q} &= 0 \end{aligned} \quad (5)$$

Here, $\wp(y)$ represents the combined influence of thermal generation and recombination processes. $G_{l,q}$ denotes the optical generation rate. $n(y)$ and $p(y)$ indicate the electron and hole concentrations, respectively, while \mathcal{D}_n and \mathcal{D}_p represents the electron and hole diffusion coefficients. The incident radiation is assumed to be uniform, and the TCAD simulator inherently solves both continuity equations [13, 14].

Transport equations

The current density for the proposed InGaAs/InP-based QWP can be expressed [15]

$$J = q\tau(\mathcal{A}1n + \mathcal{B}1n^2 + \mathcal{C}1n^3) + J_{\text{leakage}} \quad (6)$$

where $\mathcal{A}1$, $\mathcal{B}1$, and $\mathcal{C}1$ correspond to SRH, radiative, and Auger recombination coefficients, respectively, J_{leakage} is the leakage current, and ' τ ' is active layer thickness of quantum well.

Device Photocurrent

The device photocurrent for the proposed study was expressed as the product of the carrier generation rate, charge, and the bias-dependent transport efficiency, $\xi(V)$ as [16]

$$I_D = q \frac{B_n \lambda}{hc} \sum_{i=1}^{N_R} w_R \int_0^{y_i} P_i \alpha_i e^{-\alpha_i y} \xi(V) dy \quad (7)$$

where B_n is the intensity of the n th beam, λ the source wavelength, WR the width of the ray, α_i represents the absorption coefficient, N_R the number of rays traced, P_i is the attenuation before the ray starts, Y_i is the ray length.

Quantum Absorption Efficiency (η)

The overall quantum efficiency of the proposed photodetector was formulated in terms of conversion efficiency and photoconductive gain as [5].

$$\eta(\lambda, V) = \eta_{\text{abs}} \xi(V) \quad (8)$$

Detector Responsivity (R)

The detector responsivity were formulated as [5]

$$R(\lambda, V) = \eta_{\text{abs}}(\lambda) g(V) \frac{q\lambda}{hc} \quad (9)$$

$$g(V) = \frac{\tau_{\text{life}}}{\tau_{\text{tr}}(V)} = \frac{\tau_{\text{life}} v_d(V)}{Ld}$$

where $v_d(V) = \frac{\mu E}{\sqrt{1 + (\frac{\mu E}{v_s})^2}}$, here v_s is saturation velocity

and E is the applied electric field

Dark Current (I_d)

The noise current generated by the photodetector without illumination is called dark current and for the proposed InGaAs/InP-based QWP, this is formulated as [17]

$$I_{\text{dark}} = A e n_{2D} V_d(v) \quad (10)$$

Detectivity (D^*)

The detectivity of a detector with active area A_d , can be defined as the inverse of the Noise Equivalent Power (NEP) and the NEP of a detector strongly depends on the measurement of its bandwidth (Δf) [1, 18].

$$D^* = \frac{(A_d \times \Delta f)^{1/2}}{NEP} = \frac{cm\sqrt{Hz}}{W}, \quad (11)$$

where $NEP = \frac{I_n}{R}$, I_n = noise current and can be expressed as $I_n = \sqrt{4eGI_p\Delta f}$, G = optical gain and R = responsivity.

Optimization Algorithm

The performance optimization of the proposed InGaAs/InP-based QWP is formulated as a multi-objective problem to determine optimal structural and electrical parameters. The design variables were considered as

$$X = [L_w, L_b, x, V], \quad (12)$$

Subject to the constraints

$$55\text{\AA} \leq L_w \leq 62\text{\AA}, \quad \& \quad 380\text{\AA} \leq L_b \leq 420\text{\AA}, \quad 0.29 \leq x \leq 0.36, \quad \text{and} \quad -3.5 \leq V \leq 3.5$$

The objective is to simultaneously maximize quantum efficiency (η), responsivity (R), and detectivity (D^*) while minimizing dark current (I_d) and noise equivalent power (NEP), expressed as [9, 19]

Maximize: η , R , & D^* and Minimize: I_d , NEP

Further, the normalized fitness function of the proposed device was defined as

$$F = \sum_{k=1}^5 w_k \cdot f'_k, \quad \sum w_k = 1, \quad (13)$$

where f'_k are normalized objective functions.

Hybrid NSGA-II-PSO Algorithm

A hybrid NSGA-II-PSO algorithm is employed to solve the above problem. Initially, a population of candidate solutions is generated within the defined bounds. For each solution, the objective parameters are evaluated and fitness is computed [9, 19].

NSGA-II performs non-dominated sorting and crowding distance-based selection to identify elite solutions and maintain diversity. PSO is then used to update particle positions and velocities.

$$V_i^{t+1} = w \cdot V_i^t + c_1 r_1 (P_{best,i} - X_i^t) + c_2 r_2 (G_{best} - X_i^t) \quad (14)$$

$$\text{and } X_i^{t+1} = X_i^t + V_i^{t+1}. \quad (15)$$

In the above equations, V_i^t and X_i^t represent the velocity and position of the i^{th} particle at iteration t respectively. V_i^{t+1} and X_i^{t+1} denote the updated velocity and position. The parameter w is the inertia weight that controls the influence of the previous velocity. c_1 and c_2 are the cognitive and social acceleration coefficients, respectively. r_1 and r_2 are uniformly distributed random numbers in the range [0,1]. $P_{best,i}$ is the best position previously visited by the i^{th} particle, while G_{best} represents the best solution obtained among all particles in the population.

The iterative process continues until convergence, yielding the optimal design parameters:

$$L_w = 60 \text{\AA}, \quad L_b = 400 \text{\AA}, \quad x = 0.34.$$

And yielding maximum responsivity and detectivity with minimum dark current and NEP, demonstrating superior performance compared to other optimization techniques.

Table 1: Material Properties used in the computational analysis [20-26].

| Parameter | Values |
|--|--|
| Effective mass in the well | $m_w^* = 0.041m_0$ |
| Effective mass in the barrier | $m_b^* = 0.0410 + 0.0835x)m_0$, where m_0 represents the electron rest mass |
| Potential Barrier Height | $\Delta E = \frac{V}{-} = 0.75x$, where x represents the 'In' mole fraction |
| Carrier Density (well) | $1.53 \times 10^{24} \text{ cm}^{-3}$ |
| Photoconductive gain | 0.774 |
| Lorentzian profile | $\Delta E = 5 \text{ meV}$ |
| Electron mobility (μ_e) (m^2/Vs) | $10,000 \text{ cm}^2 \cdot \text{V}^{-1} \cdot \text{s}^{-1}$ |
| Electron affinity (eV) | 4.23 |
| Energy bandgap (E_g) (eV) | $(1.344 - 0.738y + 0.138y^2) \text{ eV}$ |
| Absorption coefficient (α) | $\alpha_0 \exp\left(\frac{\delta(E-E_0)}{ET}\right) (\text{m}^{-1})$ |
| Static Dielectric constant (ϵ_s) | $12.5 + 1.44Asy$ |
| High frequency dielectric constant | $9.61 + 2.0Asy$ |
| Lattice constant | 5.869\AA |

3. Results and discussion

Numerical simulations were carried out for a symmetrical and staggered In_xGa_{1-x}As/InP-based QWP structure using MATLAB. The computations were performed at a temperature of 77 K, with an applied electric field of 12.4 kV/cm across the device structure. The applied bias was varied between -3.5 V and +3.5 V, and the incident radiation was modeled to strike at an angle of 45° from the lower bandgap (InGaAs) side of the structure. The photodetector configuration under investigation

is presented in Figure 1, and the various physical parameters used in the analysis were taken from the cited references [20-26] and are abstracted in Table 1.

The TMM was employed to calculate the quantized energy levels in the quantum well. These results were used to estimate the corresponding absorption wavelengths across the THz spectral region. The subband energy levels of the quantum well corresponding to the transmission coefficient peaks were plotted for well widths ranging from 55 Å to 62 Å and for Indium (In) mole fractions (x) varying between 0.29 and 0.36.

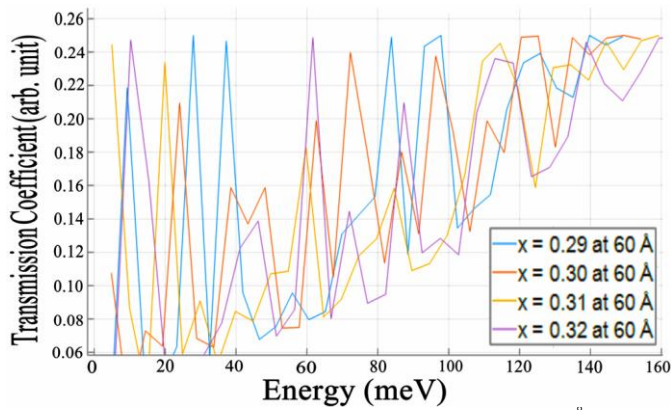


Figure 3: Transmission coefficient vs. energy at $L_w = 60 \text{ \AA}$ for $x = 0.29$ to 0.32 .

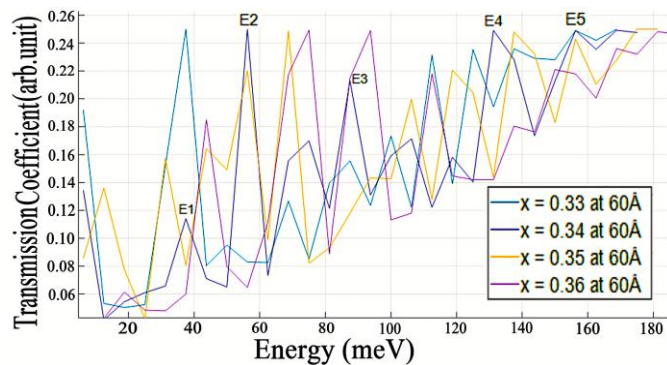


Figure 4: Transmission coefficient vs. energy at $L_w = 60 \text{ \AA}$ for $x = 0.33$ to 0.36 .

Figure 3, 4, and 5 present a detailed analysis of the transmission coefficient profiles, highlights the variation in Indium (In) composition in the well material $\text{In}_x\text{Ga}_{1-x}\text{As}$ from $x = 0.29$ to 0.36 and its influence on the energy-dependent transmission at a quantum well width of 60 \AA . The energy positions of the transmission peaks were then used to extract the corresponding sub-band energy levels, facilitating the estimation of the material’s bandgap energy. This evaluated bandgap was then utilized to determine the operational wavelength of the proposed photodetector for different well widths and ‘In’ mole fractions. The most prominent detection feature occurs for $L_w=60 \text{ \AA}$ and $x = 0.34$, as illustrated in Figure 5 [27, 28].

Figure 6 presents the variation of wavelength corresponding to the calculated sub-band energy levels, derived from the transmission coefficient spectra, as a function

of the Indium (In) mole fraction for quantum well widths of 55 \AA , 56 \AA , 58 \AA , 60 \AA , and 62 \AA . The operating wavelengths for each mole fraction (x) and well width are summarized in Table 2. From Figure 6 and Table 2, it is evident that the $\text{In}_x\text{Ga}_{1-x}\text{As}/\text{InP}$ -based QWP exhibits operation around 28.2 THz , which corresponds to energy values of approximately 156.25 meV and 38.5 meV . At this configuration, the computed energy gap is 117.7 meV , and the associated wavelength for the conduction band offset is about 10.58 \mu m , as indicated in Figure 5. In this case, the detector structure has a well width of 60 \AA and an Indium mole fraction of 0.34 . The obtained results show good agreement with previously reported studies [4, 29, 30]. Furthermore, the proposed InGaAs/InP -based QWP structure demonstrates strong correlation with the experimental data reported by Min-Su Park et al. (2018), confirming its feasibility for practical fabrication and real-world applications [4].

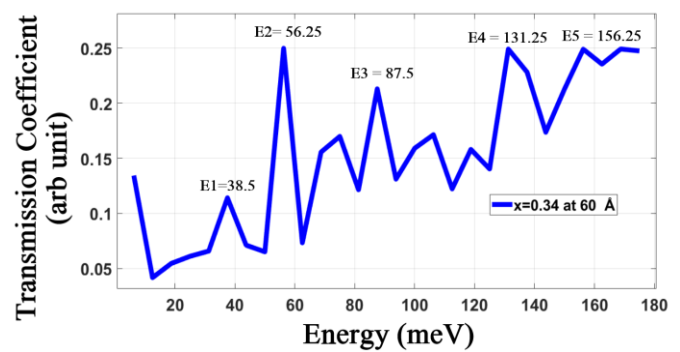


Figure 5: Transmission coefficient vs. energy at $L_w = 60 \text{ \AA}$ for ‘In’ mole fraction, $x = 0.34$.

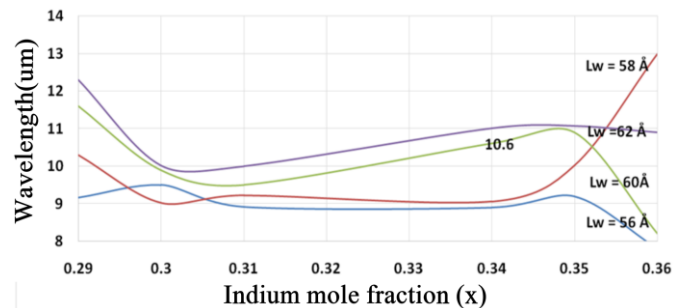


Figure 6: Wavelength (λ) vs. ‘In’ mole fraction (x) at well widths (L_w) 56 \AA , 58 \AA , 60 \AA , and 62 \AA .

Table 2: Absorption efficiency, responsivity, and wavelength values for various well widths (L_w) and Indium mole fractions (x), derived from Figures 3 to 8

| Well width (L_w in \AA) | Indium mole fraction (x) | Wavelength λ_{peak} (μm) | Absorption Efficiency (η) cm^{-1} | Responsivity (A/W) |
|--------------------------------------|------------------------------|--|---|-------------------------------|
| 55 | 0.31 | 8.9 | 700 | 2.52 |
| 56 | 0.31 | 9.02 | 760 | 2.54 |
| 58 | 0.29 | 9.2 | 850 | 2.50 |
| 60 | 0.34 | 10.6 | 945 | 2.70 |
| 62 | 0.35 | 11.6 | 997 | 2.78 |

Hence the variation in operating wavelength with Indium mole fraction and quantum well width demonstrates the strong dependence of the detector’s spectral response on structural parameters. Increasing Indium concentration leads to a narrower bandgap and hence a shift toward longer wavelengths, while decreasing well width enhances quantum confinement, producing a blueshift. This tunability highlights

the potential of $\text{In}_x\text{Ga}_{1-x}\text{As}/\text{InP}$ quantum well structures for application in the terahertz and mid-infrared spectral regions, where wavelength selectivity is critical for device optimization. The computed results align closely with earlier theoretical and experimental findings, validating the simulation approach [31, 32].

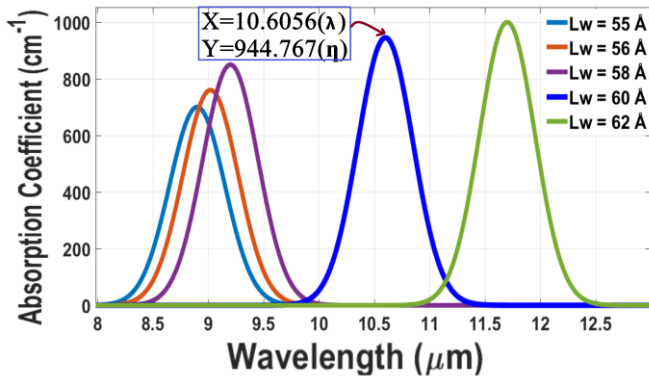


Figure 7: Absorption coefficient (η) vs. wavelength (λ) at various well width $L_w = 55 \text{ \AA}$ to 62 \AA and at 'In' mole fraction $x = 0.34$.

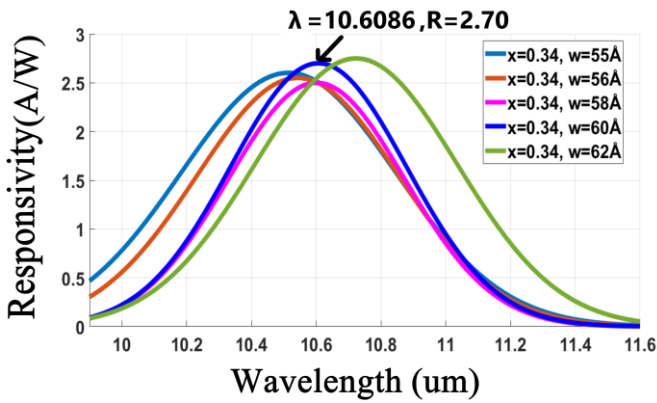


Figure 8: Responsivity vs. wavelength at various well width and 'In' mole fraction at bias voltage -3V .

In this study, Figure 7 presents the absorption efficiency of the proposed structure, simulated as a function of wavelength for different well widths ranging from 55 \AA to 62 \AA , while keeping the Indium (In) composition fixed at 0.34 . The analysis reveals that the absorption efficiency peak tends to increase with increasing quantum well width [5, 33]. For $L_w = 60 \text{ \AA}$, the maximum absorption efficiency is obtained for an Indium mole fraction of $x = 0.34$, corresponding to a wavelength of 10.6 \mu m with an efficiency value of 945 cm^{-1} [34].

Figure 8 presents the variation of responsivity (R) with operating wavelength (λ), highlighting the influence of quantum well width and Indium mole fraction (x) on the overall detector performance. The analysis shows that a comparatively high responsivity of 2.7 A/W is obtained at $x = 0.34$ under a bias voltage of -3.0 V . Such enhanced responsivity can be achieved through the careful optimization of both the Indium composition and the quantum well width. Furthermore, the results indicate that the peak responsivity increases progressively with larger well widths and higher Indium concentrations [29].

Further, Figure 9 shows the variation of dark current with applied bias for different Indium concentrations and quantum well widths. For the proposed QWP structure, a low dark current of 68 nA is obtained at an applied bias of -3.0 V for $x = 0.34$ and $L_w = 60 \text{ \AA}$. This result is consistent with the expected characteristics of the $\text{In}_x\text{Ga}_{1-x}\text{As}/\text{InP}$ quantum well photodetector, considering both the material parameters and the applied bias conditions, and aligns closely with values reported in earlier literatures [6, 26].

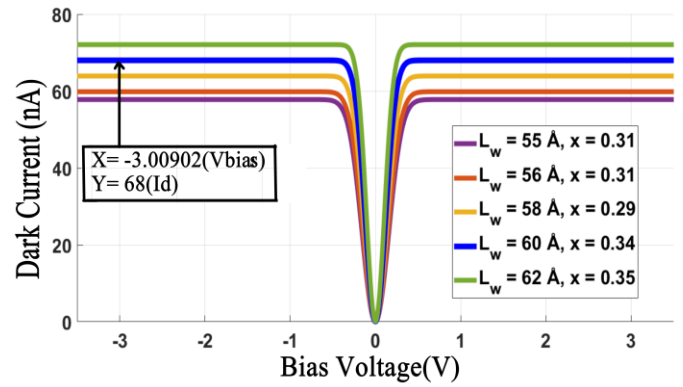


Figure 9: Dark Current vs. bias voltage at different 'In' mole fraction and well width (L_w).

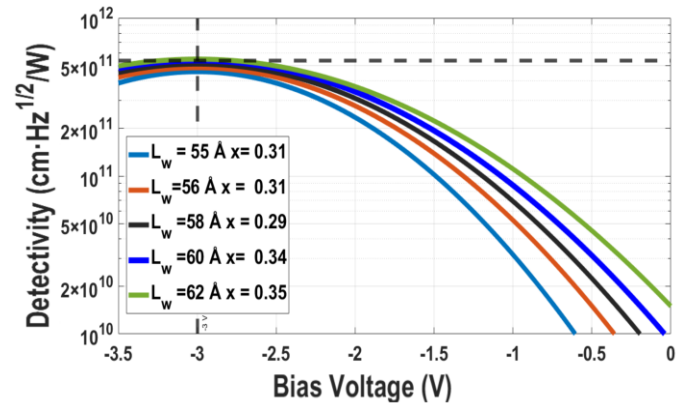


Figure 10: Detectivity vs. bias voltage at different 'In' mole fraction and well width (L_w).

Figure 10 illustrates the specific detectivity that can be achieved for $\text{In}_x\text{Ga}_{1-x}\text{As}/\text{InP}$ QWP for various selected well width and 'In' mole fraction. High detectivity indicates the potentiality of a photodetector to detect weak incident optical signals. Detectivity and responsivity of any photodetector are directly related to each other according to the mathematical expression (18 & 19). For the photosensitive area A_d and the bandwidth (Δf), this is usually considered as 1 Hz for the calculation [35]. It can be concluded from equations (15, 16, & 19) that low dark current and high responsivity are desired for any photodetector to manifest high detectivity. Figure 10 shows the estimated detectivity of the proposed device as a function of reverse bias voltage between -3.5 to 0 volt variation. For a specific wavelength of 10.6 \mu m the simulated result of detectivity is obtained as $5.38 \times 10^{11} \text{ cm}^2 \sqrt{\text{Hz}} \text{ W}^{-1}$ under -3 volt bias and at $L_w = 60 \text{ \AA}$ and $x = 0.34$, represented in Figure 11. A substantial enhancement in specific detectivity is observed in this work compared to previously reported quantum well photodetectors. [6, 29].

Furthermore, the calculated values of dark current, and detectivity, for different quantum well widths (L_w) and Indium molar concentrations (x) are listed in Table 3, derived from the results shown in the preceding figures. A comparison of Tables 2 and 3 indicates that, for the proposed QWP structure, an increase in well width leads to a corresponding rise in the absorption coefficient, and with a higher Indium content, the peak wavelength shifts toward shorter wavelength values within the terahertz region. For $x = 0.34$, the detector operates at 28.2 THz (10.6 \mu m), resulting in enhanced responsivity, and detectivity, along with reduced dark current.

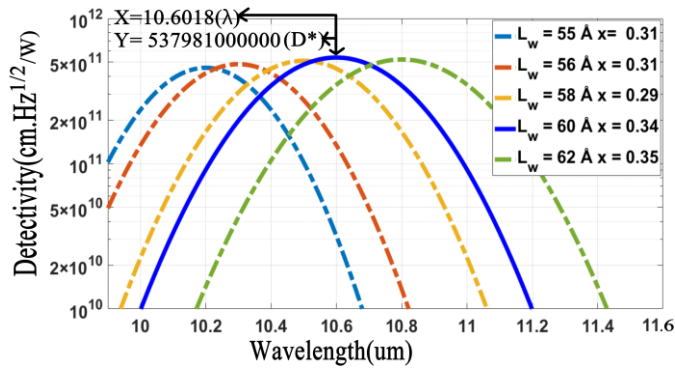


Figure 11: Detectivity vs. wavelength under the bias of -3.0 V at 77K.

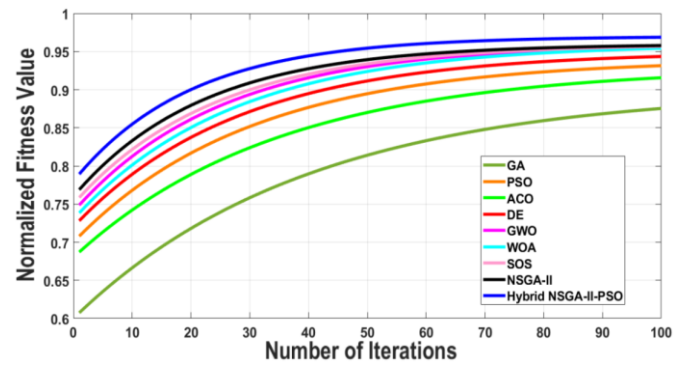


Figure 12: Convergence of metaheuristic algorithms showing superior performance of the Hybrid NSGA-II-PSO.

Table 3: Dark Current, and Detectivity values, for various well widths (L_w) and Indium mole fractions (x), derived from Figs. 9 to 11.

| Well width (L_w in Å) | Indium mole fraction (x) | Wavelength λ_{peak} (μm) | Dark current (nA) | Detectivity ($cm\sqrt{Hz}W^{-1}$) |
|--------------------------|------------------------------|---|-------------------|-------------------------------------|
| 55 | 0.31 | 8.9 | 58 | 0.32×10^{11} |
| 56 | 0.31 | 9.02 | 60 | 1.35×10^{11} |
| 58 | 0.29 | 9.2 | 63 | 4.48×10^{11} |
| 60 | 0.34 | 10.6 | 68 | 5.38×10^{11} |
| 62 | 0.35 | 11.6 | 72 | 3.52×10^{11} |

To further enhance the device performance, a comprehensive multi-objective optimization study was carried out using various metaheuristic algorithms, including GA, PSO, DE, GWO, WOA, SOS, and ACO. The optimization simultaneously maximizes quantum efficiency, responsivity, and detectivity, while minimizing dark current and noise equivalent power (NEP) [19, 36-40]. The comparative analysis reveals that all algorithms converge toward improved device performance; however, noticeable variations are observed in convergence accuracy and stability. Among them, the hybrid

NSGA-II-PSO algorithm demonstrates superior optimization capability by effectively balancing exploration and exploitation, leading to the optimal design parameters $L_w = 60 \text{ \AA}$, $L_b = 400 \text{ \AA}$, and $x = 0.34$. At this configuration, the device achieves a high responsivity of 2.7 A/W, enhanced detectivity of $5.38 \times 10^{11} \text{ cm}\sqrt{\text{Hz}}W^{-1}$, and a reduced dark current of 68 nA, along with minimized NEP. These results confirm the effectiveness of the hybrid optimization approach in achieving an optimal trade-off among conflicting performance parameters for high-sensitivity THz photodetection.

Table 4. Comparative evaluation of device performance parameters obtained using various metaheuristic optimization algorithms for the proposed InGaAs/InP QWP.

| Algorithm | Absorption Efficiency (η) cm^{-1} | Responsivity (A/W) | Detectivity ($cm\sqrt{Hz}W^{-1}$) | Dark current (nA) | NEP (w/\sqrt{Hz}) | Convergence |
|--------------------|--|--------------------|-------------------------------------|-------------------|------------------------|-------------|
| GA | 900 | 2.45 | 4.60×10^{11} | 82 | 2.25×10^{-12} | slow |
| PSO | 920 | 2.56 | 4.86×10^{11} | 77 | 2.10×10^{-12} | good |
| ACO | 928 | 2.51 | 4.72×10^{11} | 80 | 2.18×10^{-12} | moderate |
| DE | 936 | 2.61 | 4.88×10^{11} | 74 | 2.02×10^{-12} | good |
| GWO | 932 | 2.63 | 5.08×10^{11} | 73 | 1.95×10^{-12} | good |
| WOA | 937 | 2.58 | 5.02×10^{11} | 74 | 1.98×10^{-12} | good |
| SOS | 940 | 2.65 | 5.27×10^{11} | 71 | 1.92×10^{-12} | better |
| NSGA-II | 942 | 2.68 | 5.35×10^{11} | 69 | 1.85×10^{-12} | Very good |
| Hybrid NSGA-II-PSO | 946 | 2.70 | 5.39×10^{11} | 68 | 1.82×10^{-12} | Best |

From Table 4, the optimized device parameters ($L_w = 60 \text{ \AA}$ and $x = 0.34$) obtained through the hybrid NSGA-II-PSO algorithm yield a maximum responsivity of 2.7 A/W, detectivity of $5.39 \times 10^{11} \text{ cm}\sqrt{\text{Hz}}.W^{-1}$, and a minimum dark current of 68 nA. Comparative analysis with other

metaheuristic algorithms demonstrates that they converge to sub-optimal solutions with relatively lower responsivity and detectivity and higher noise characteristics. The employed optimization algorithms are based on well-established metaheuristic techniques reported in literature [19, 36-40].

Table 5: Comparison of optimized well width, barrier width, and Indium mole fraction for the proposed InGaAs/InP QWP using different metaheuristic algorithms.

| Algorithm | Well width (L_w) | Barrier width (L_b) | Mole fraction (x) | Normalised fitness |
|--------------------|----------------------|-------------------------|-----------------------|--------------------|
| GA | 55-62 | 380 | 0.30-0.36 | 0.89 |
| PSO | 57-61 | 390 | 0.31-0.36 | 0.94 |
| ACO | 58-61 | 385 | 0.30-0.35 | 0.92 |
| DE | 59-61 | 385 | 0.32-0.34 | 0.95 |
| GWO | 57-62 | 397 | 0.32-0.36 | 0.96 |
| WOA | 57-61 | 395 | 0.32-0.35 | 0.93 |
| SOS | 59-63 | 402 | 0.33-0.34 | 0.96 |
| NSGA-II | 58-60 | 398 | 0.33-0.34 | 0.97 |
| Hybrid NSGA-II-PSO | 60 ± 1 | 401 | 0.34 | 0.98 |

Table 5 presents the optimized structural parameters of the proposed QWP obtained using different metaheuristic algorithms. It is observed that the hybrid NSGA-II-PSO approach converges to the optimal design with $L_w = 60 \pm 1$ Å,

$L_b = 401$ Å, and $x = 0.34$, achieving the highest normalized fitness value, while other algorithms exhibit wider parameter variations and comparatively lower fitness as shows by Figure 12.

Table 6: Comparison of the present study with the contemporary work.

| Ref. | Material System | L_w (Å) | Molar Fraction (x) | Bias (V) | Opr. Freq. (THz) | Temp. (K) | Responsivity (A/W) | Detectivity ($\text{cm}\sqrt{\text{HzW}}^{-1}$) | Dark Current |
|--------------------------|-----------------|-----------|--------------------|--------------|------------------|-----------|--------------------|---|---|
| Min-Su Park et al [4] | InGaAs/InP | 56 | 0.53 | -0.7 | 28.2 | 77 | ----- | ----- | 8.5×10^{-8} A |
| B.F. Levine et al [29] | GaAs/AlGaAs | 38 | 0.22 | | 29.3 | 77 | 0.35 | 1×10^{11} | 10 uA |
| Jingyi Wang et al [6] | InGaAs/InP | ----- | 0.53 | -1.0 | 149.8 | 293 | ----- | 1.59×10^{10} | 3.48×10^{-4} A/cm ² |
| Mihail Giannopoulos [41] | GaAs/AlGaAs | 70 | 0.20 | -4.0 | 30 | 10 | 0.38 | 3.5×10^{11} | 1.0×10^{-9} A |
| S.V. Bandara et al [42] | GaAs/AlGaAs | 150 | 0.06 | ----- | 8.9 | 7 | --- | 1.8×10^{11} | ---- |
| Proposed work | InGaAs/InP | 60 | 0.34 | -3.5 to +3.5 | 28.2 | 77 | 2.7 | 5.38×10^{11} | 68 nA |

Table 6 presents a comparative analysis of the proposed InGaAs/InP QWP with previously reported photodetectors in terms of structural parameters and key performance metrics. It is observed that the proposed device achieves a significantly higher responsivity of 2.7 A/W and enhanced detectivity of $5.38 \times 10^{11} \text{ cm}\sqrt{\text{HzW}}^{-1}$, along with a low dark current of 68 nA at 77 K. Compared to existing works, the proposed structure demonstrates superior performance and improved sensitivity, highlighting the effectiveness of the optimized design for high-performance terahertz infrared detection.

4. Conclusions

In this work, an InGaAs/InP-based quantum well photodetector (QWP) has been designed and analyzed for long-wavelength terahertz infrared detection in the 8–12 μm range. The device performance was evaluated using both analytical modeling via the Transfer Matrix Method (TMM) and numerical simulation through TCAD, ensuring accurate prediction of energy states and carrier transport. The results indicate that the detector characteristics are strongly influenced by structural parameters, with an optimal configuration of $L_w = 60$ Å and $x = 0.34$ yielding a high responsivity of 2.7 A/W, enhanced detectivity of $5.38 \times 10^{11} \text{ cm}\sqrt{\text{HzW}}^{-1}$, and a low dark current of 68 nA. A comprehensive multi-objective optimization study confirms that the hybrid NSGA-II-PSO algorithm provides superior convergence and an optimal trade-off among performance parameters compared to other metaheuristic techniques. The novelty of this work lies in the integration of a physics-based QWP model with a hybrid metaheuristic optimization framework for simultaneous performance enhancement. However, the study is limited to simulation-based analysis under ideal conditions without experimental validation. Future work will focus on experimental realization and validation of the proposed device, along with the exploration of advanced material systems and inclusion of temperature-dependent effects and fabrication constraints to further improve practical applicability.

Authors' contributions

The author read and approved the final manuscript.

Conflicts of interest

The author declares no conflict of interest.

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Data availability

No new data were created.

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